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**N91 - 28213**

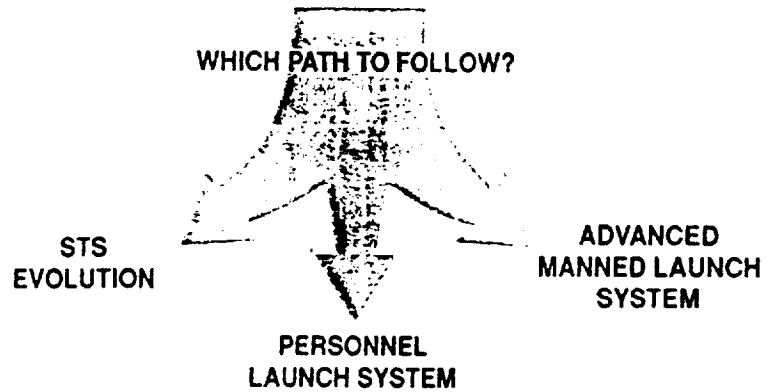
**PROPULSION STUDIES FOR  
ADVANCED MANNED LAUNCH SYSTEMS**

Vehicle Analysis Branch  
Space Systems Division  
NASA Langley Research Center

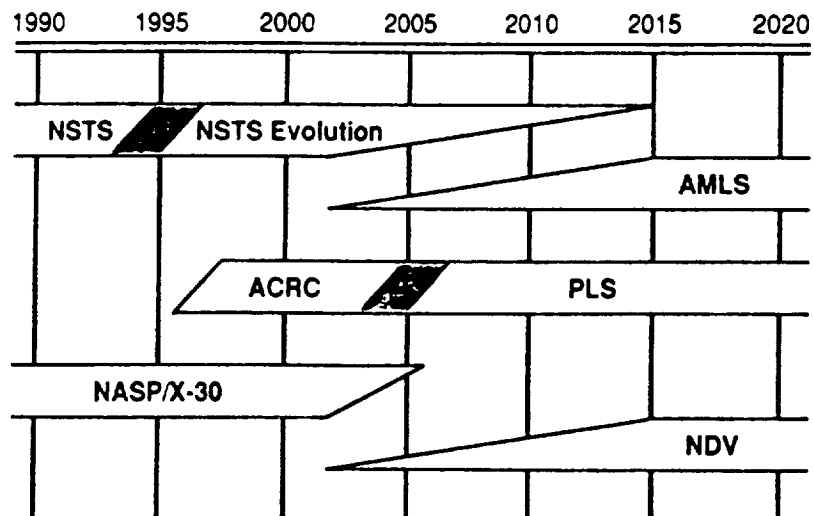
Presented by: D. Freeman

## THE NEXT MANNED SPACE TRANSPORTATION SYSTEM

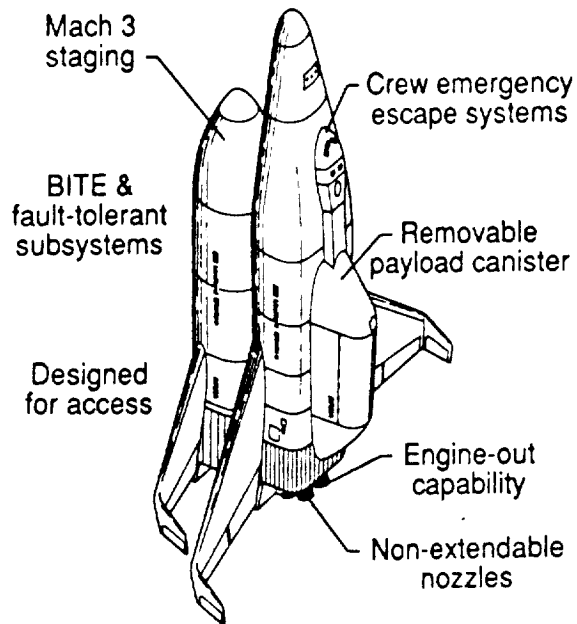
- Satisfy people/payload requirements
- Improve cost effectiveness
- Increase reliability
- Increase margins



## MANNED SPACE TRANSPORTATION OPTIONS SCHEDULE



## DESIGN FOR OPERATIONS, RELIABILITY AND SAFETY

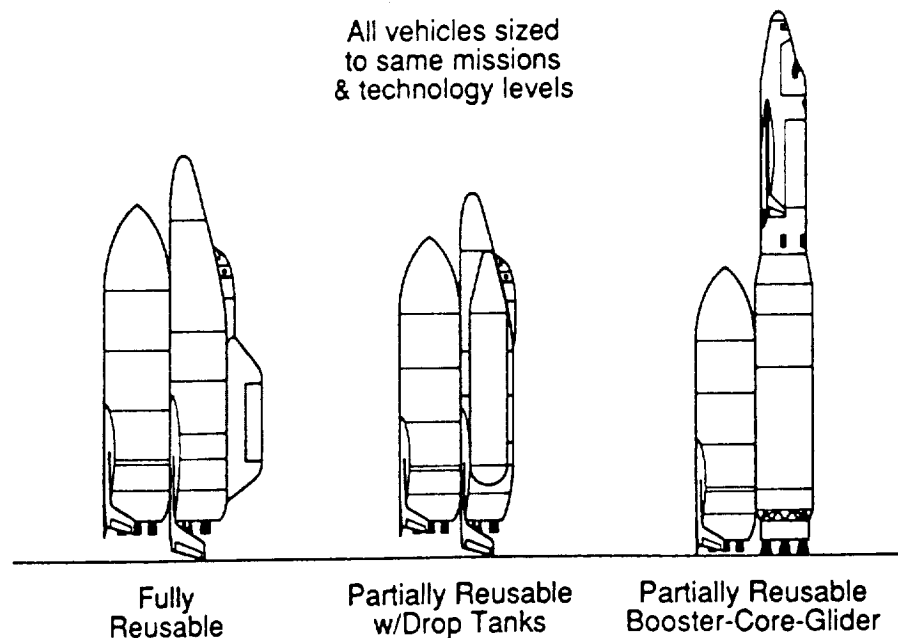


### Technology Advantage Applied to:

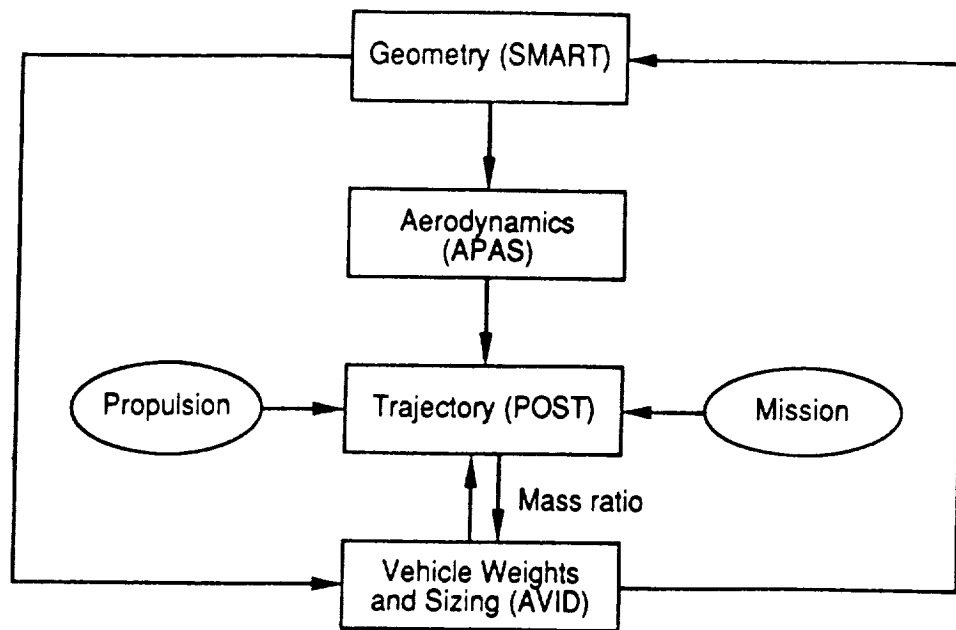
- Operations streamlining
- Robust subsystems
- Improved reliability
- Assured mission success
- Safety

**Not Maximum Payload**

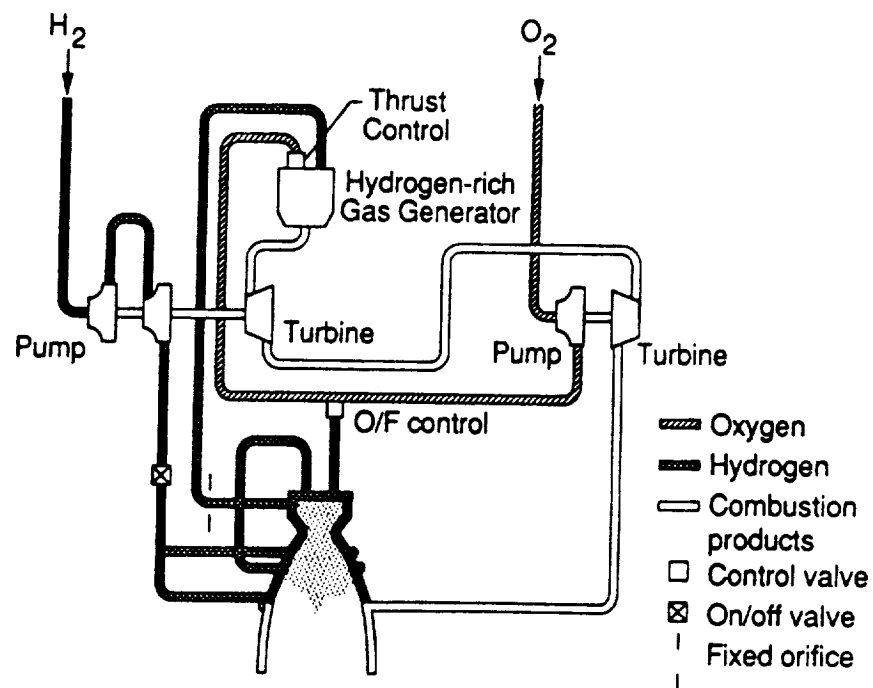
## ADVANCED MANNED LAUNCH SYSTEM CONCEPTS



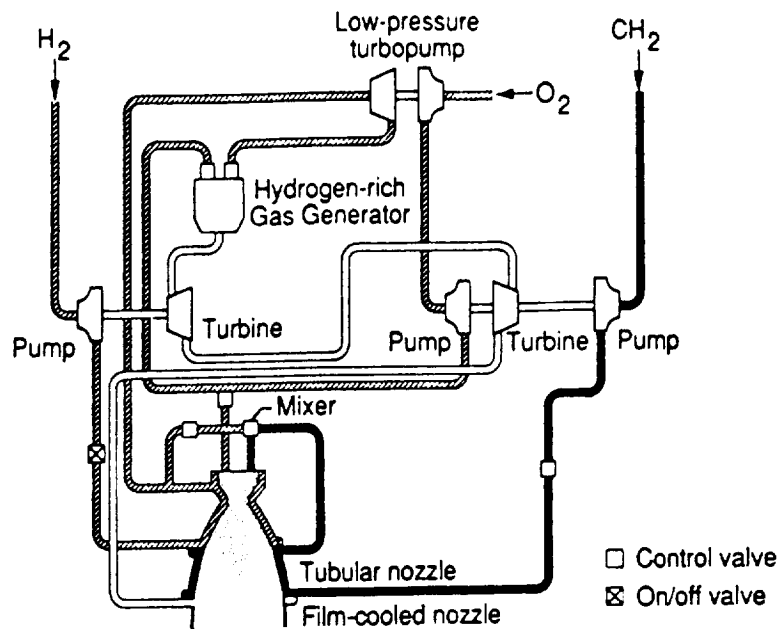
## VEHICLE DESIGN PROCESS



## REFERENCE STME ENGINE

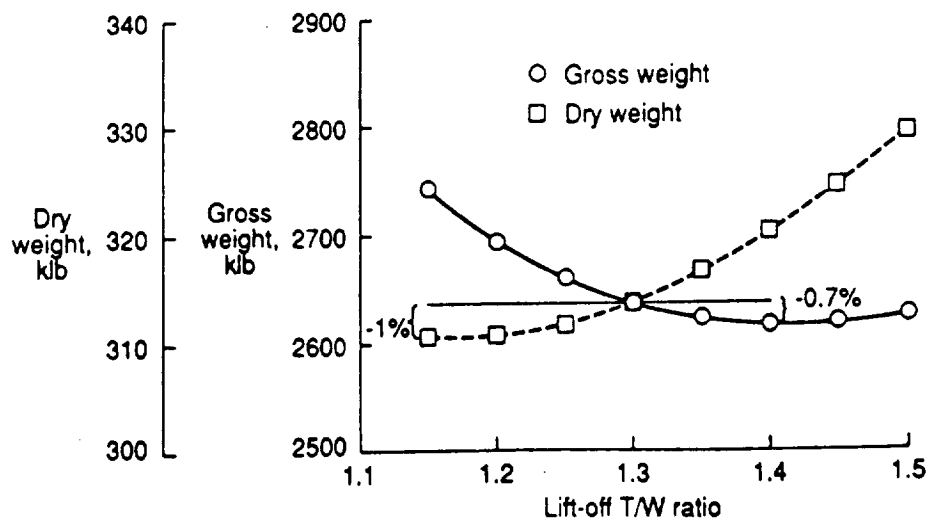


## REFERENCE STBE ENGINE



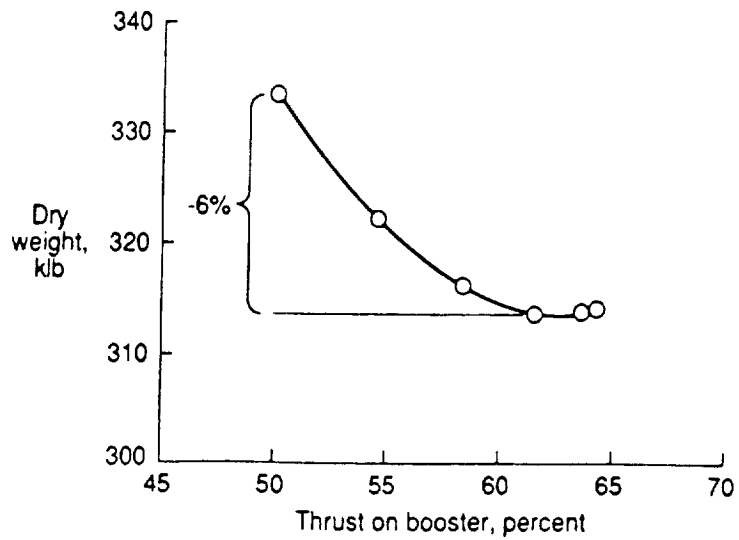
## LIFT-OFF THRUST-TO-WEIGHT TRADE

FULLY REUSABLE, ALL LOX/LH<sub>2</sub>



## THRUST SPLIT TRADE AT LIFT-OFF

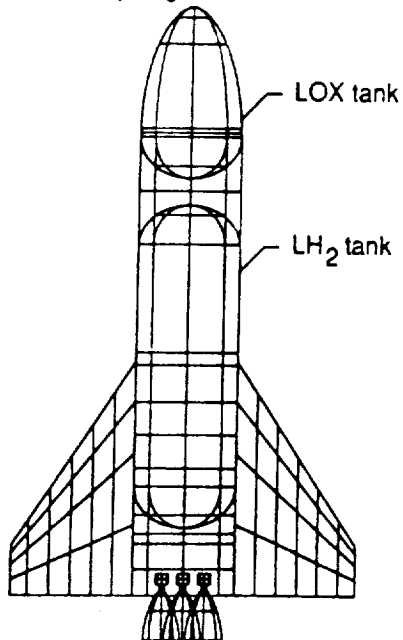
FULLY REUSABLE, ALL LOX/LH<sub>2</sub>



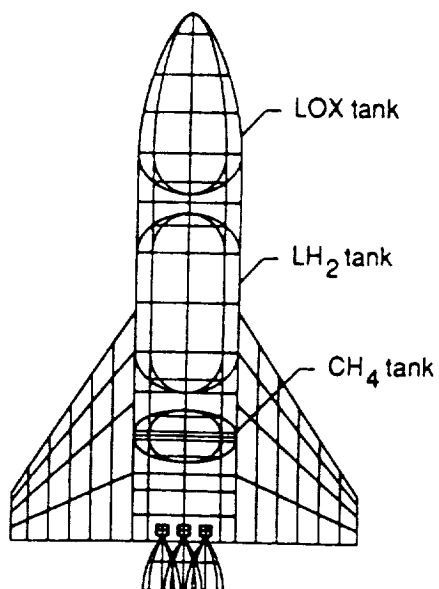
- Chose 7 engines on booster, 4 engines on orbiter

## AMLS REUSABLE BOOSTERS

Hydrogen-Fueled



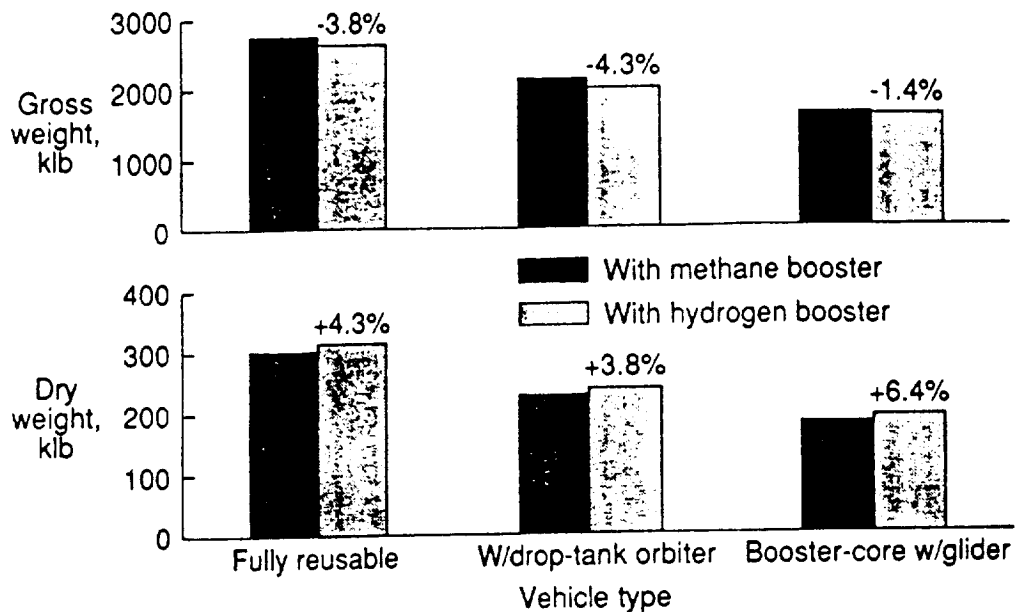
Methane-Fueled



## AMLS CONCEPT PROPULSION TRADES

### SINGLE FUEL VERSUS DUAL FUEL

- All vehicles designed to same reference mission (polar, 12 klb) and same technology level
- Boosters use methane or hydrogen as main propellant (STME/STBE engine)

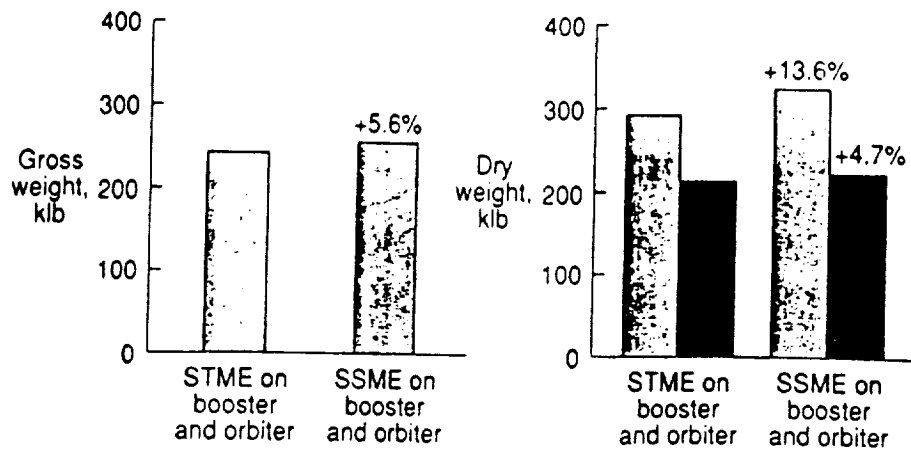


## ADVANTAGES OF THE ALL-HYDROGEN VEHICLE

- Reduced development costs
  - Delete STBE-type engine development (traded off against slightly increased vehicle dry weight)
- Reduced production costs
  - Increased line production of one type of engine
- Simpler operations
  - Common engine systems used on both stages
  - Elimination of hydrocarbon fuel and associated storage, handling, and management organization structure
- Environmental factors
  - Hydrogen fuel cleaner burning
    - Reduced engine maintenance
    - Elimination of detrimental hydrocarbon exhaust byproducts

## SSME VERSUS SINGLE-POSITION STME

FULLY REUSABLE, ALL LOX/LH<sub>2</sub> VEHICLE

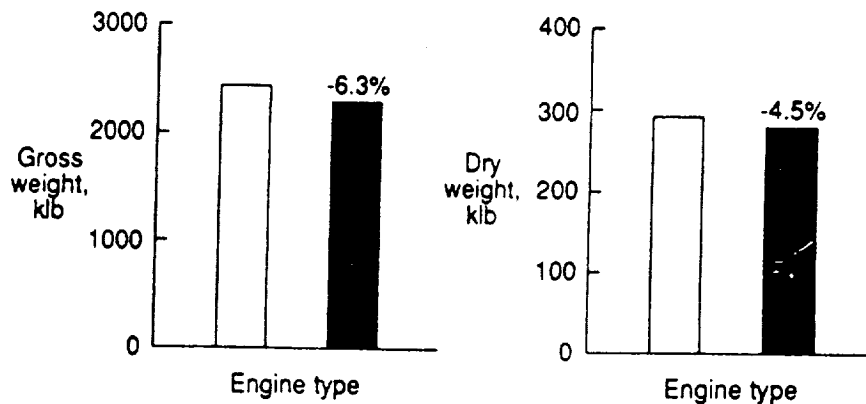


- Cases use current, unmodified SSME
- OF ratio is 6.0 for SSME and STME
- $\epsilon = 77.5$  for SSME,  $\epsilon = 60$  for STME
- Both cases have engine-out capability

□ Including propulsion weight  
 ■ Without propulsion weight

## DUAL-POSITION NOZZLE TRADE

FULLY REUSABLE, ALL LOX/LH<sub>2</sub>

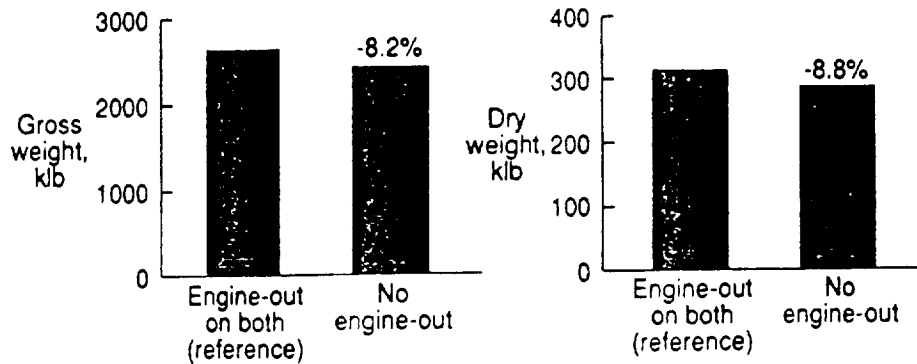


□ Single-position nozzle ( $\epsilon = 60$ ), corrected  $I_{sp}$   
 ■ Dual-position nozzle ( $\epsilon = 60/120$ ), on orbiter



## ENGINE-OUT CAPABILITY TRADE

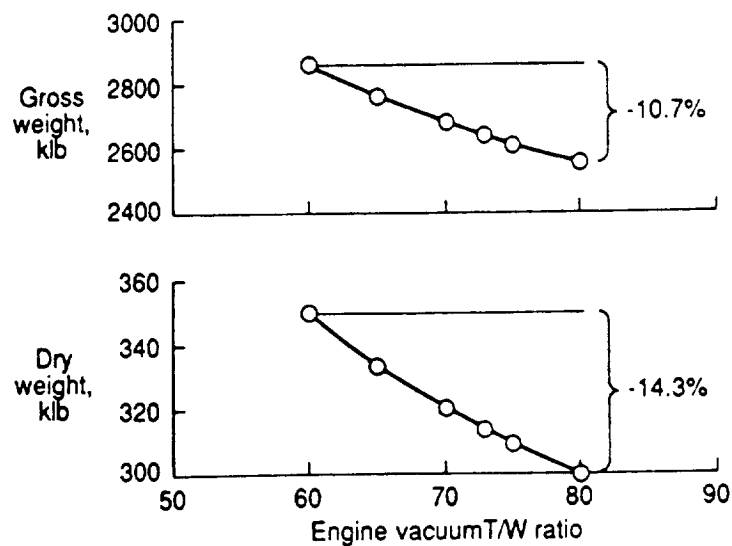
FULLY REUSABLE, ALL LOX/LH<sub>2</sub> VEHICLE



- At least 4 engines required on both the booster and orbiter
- Increased vehicle reliability brings about:
  - Quantitative reduction in recurring costs
  - Qualitative increase in crew and mission safety

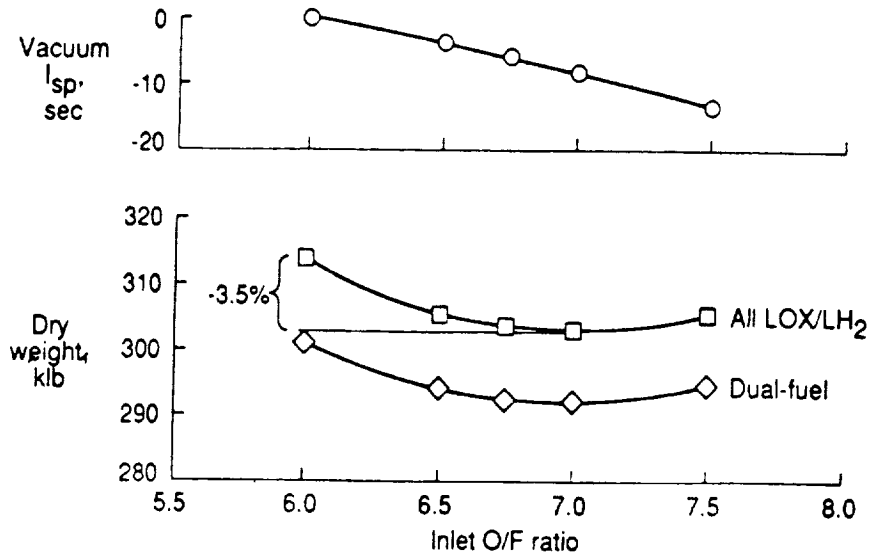
## ENGINE THRUST-TO-WEIGHT RATIO TRADE

FULLY REUSABLE, ALL LOX/LH<sub>2</sub>



- Constant O/F ratio and  $I_{sp}$  for all cases

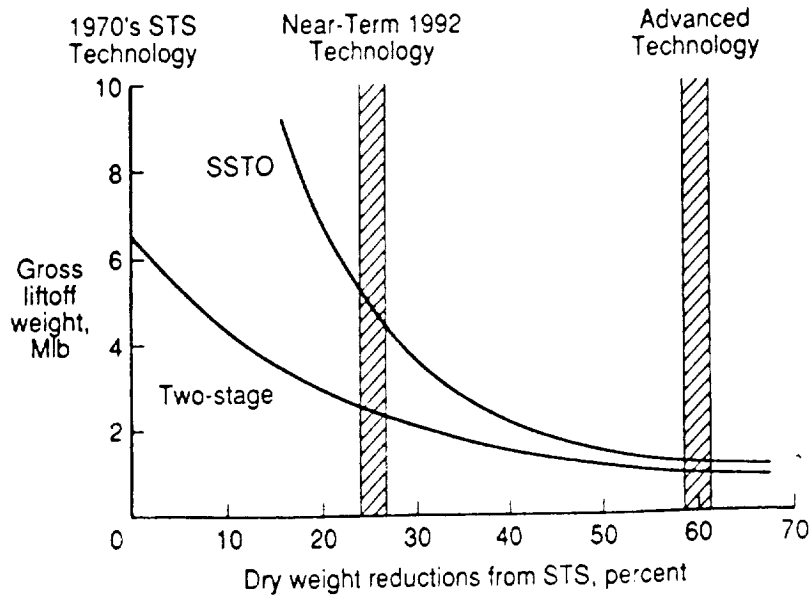
## AMLS OXIDIZER/FUEL RATIO TRADE FULLY REUSABLE



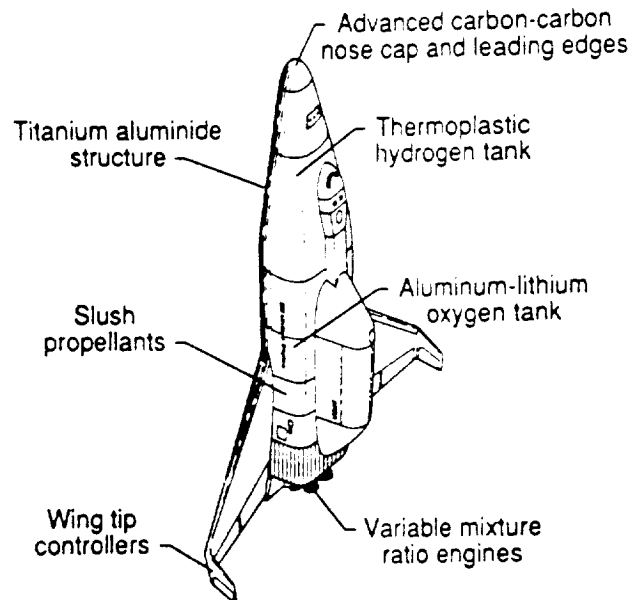
## CONCLUSIONS

- Development of a new hydrocarbon booster engine (like the STBE) for next-generation manned systems may not be cost effective
- Development of a new hydrogen engine (like the STME) for next-generation manned systems could prove cost effective for use as a main (and booster) propulsion system
- Use of a dual-position nozzle would probably not be beneficial for a design-for-operations system like AMLS
- An increase in oxidizer-to-fuel ratio from the current SSME level of 6 to approximately 7 would be beneficial in reducing future launch system weights

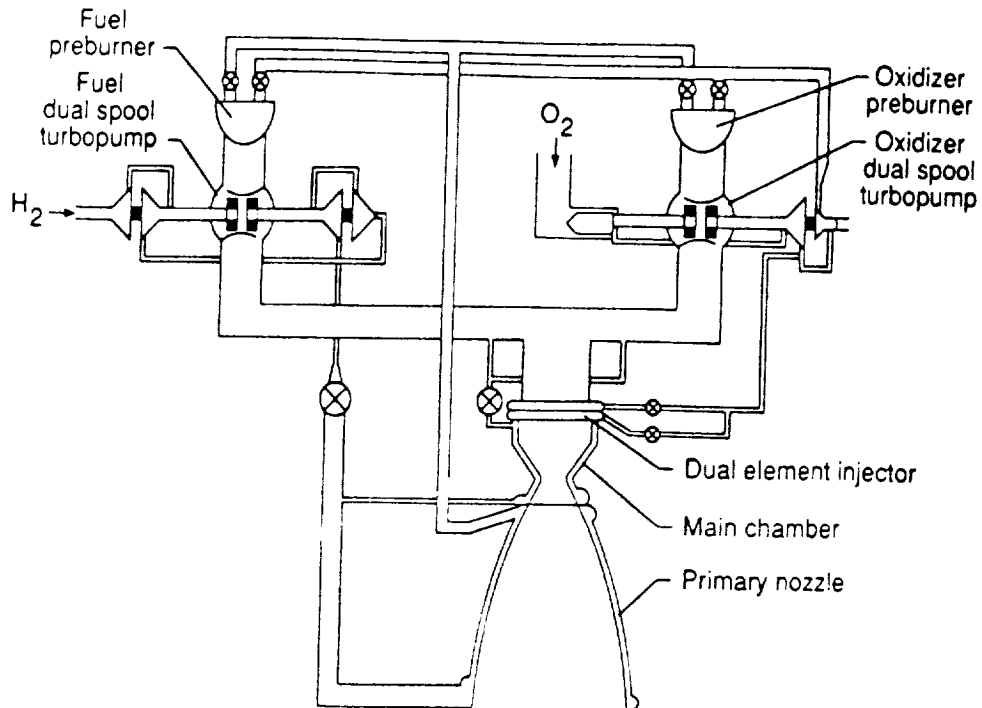
## TECHNOLOGY EFFECT ON ROCKET LAUNCH VEHICLE WEIGHT



## ADVANCED SSTO VEHICLE TECHNOLOGIES



## PRATT & WHITNEY VMR FLOW SCHEMATIC



## ADVANCED VARIABLE-MIXTURE RATIO ENGINE

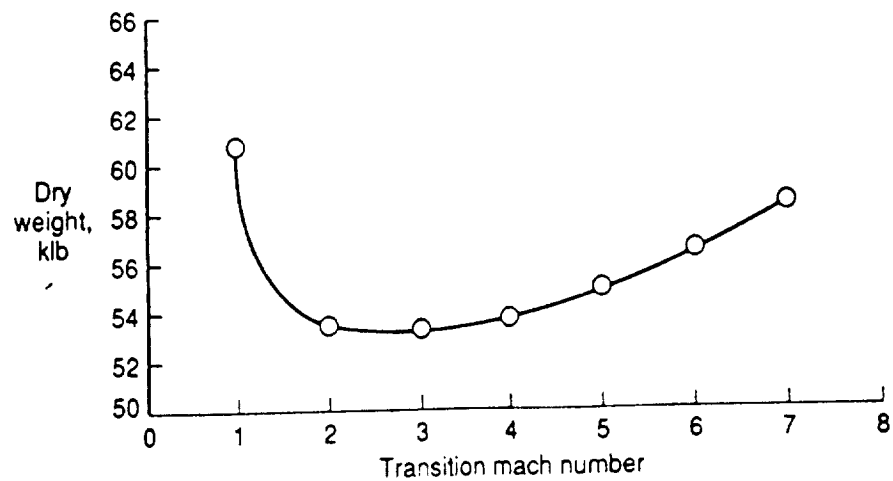
### HYDROGEN/OXYGEN

Mode	1	2	SSME (109%)
O/F Ratio	12	6	6.026
Nozzle	Retracted	Extended	Single-position
Expansion Ratio	40	150	77.5
Vacuum Thrust, lb	254,500	176,900	512,300
Vacuum Isp, sec	362	467	452
Chamber Press., psia	4,000	2,700	3260
SL Thrust, lb	234,580	142,832*	417,300
SL Thrust/Weight	109.5	66.68*	60

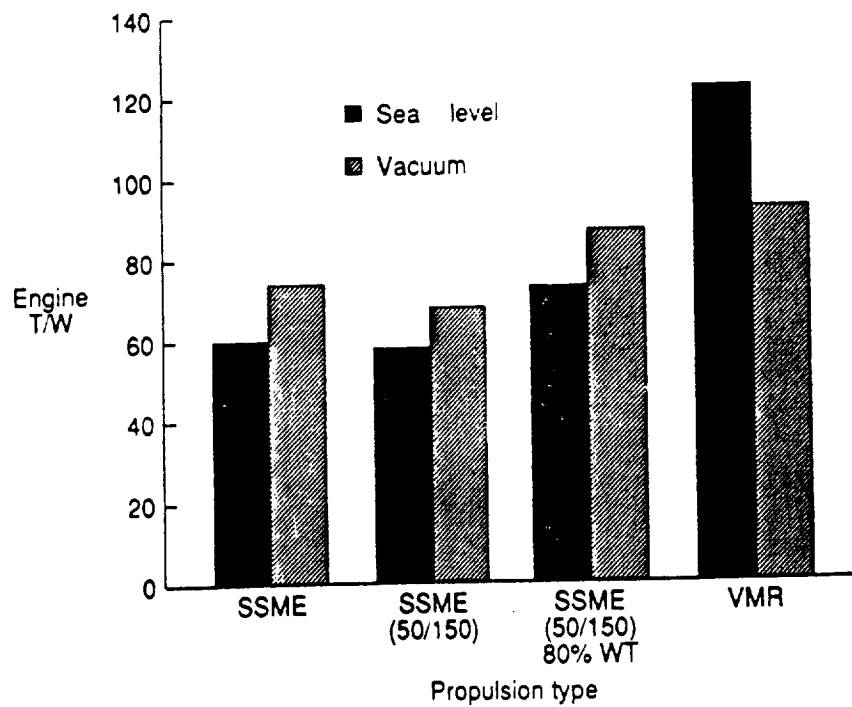
\*Area ratio of  $\epsilon = 40$

## TRANSITION MACH NUMBER TRADE (VMR ENGINE)

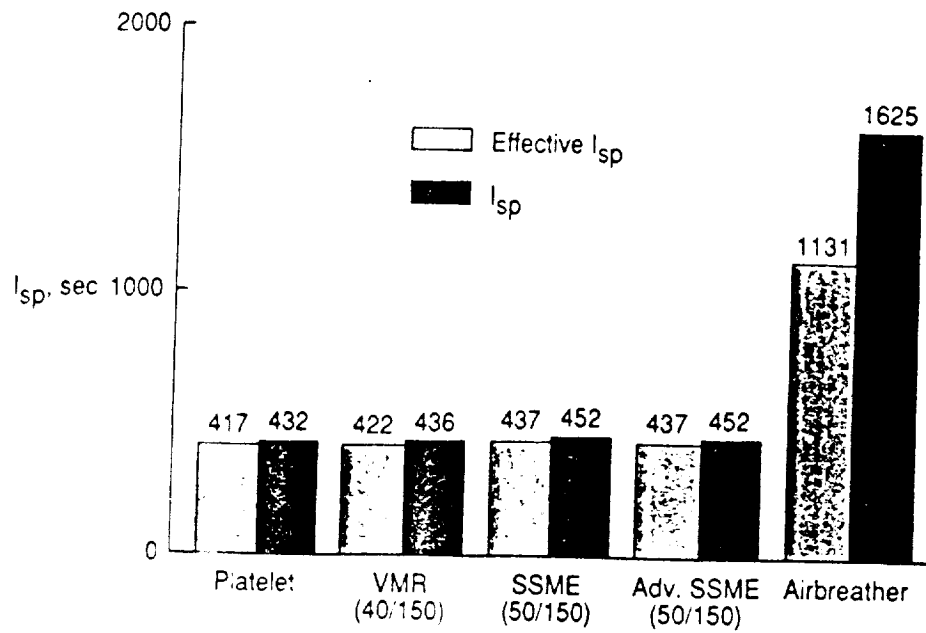
INITIAL TRADE



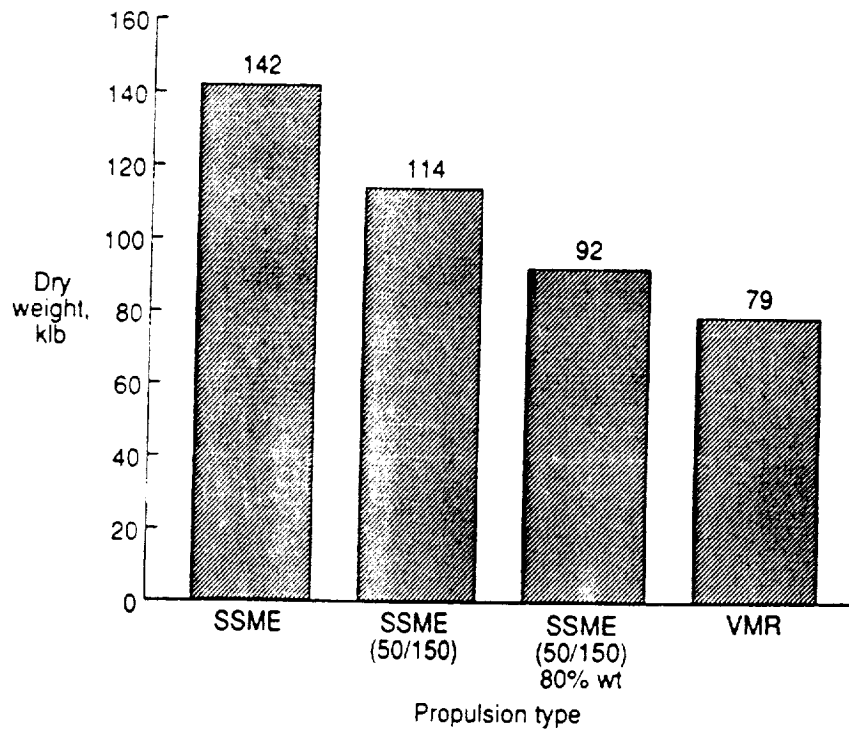
## COMPARISON OF PROPULSION CHARACTERISTICS



### TIME AVERAGED SPECIFIC IMPULSE



### DRY WEIGHT SENSITIVITY TO PROPULSION TYPE



## CONCLUSIONS

- Application of advanced technologies could allow introduction of rocket-powered SSTO vehicle for 2015 IOC
  - Low dry weight compared to two-stage and airbreathers
  - Lower operation costs than two-stage
- Application of variable-mixture-ratio technology and cooled, vaneless turbines could greatly benefit advanced vehicles
  - Lower specific impulse
  - Higher T/W ratio
  - Higher bulk density





**PRESENTATION 1.3.9**

**NATIONAL AEROSPACE PLANE (NASP)**

